

AD

SPECIAL PUBLICATION ARCCB-SP-00013

**INDEX TO BENET LABORATORIES
TECHNICAL REPORTS - 1999**

R. D. NEIFELD

JULY 2000



**US ARMY ARMAMENT RESEARCH,
DEVELOPMENT AND ENGINEERING CENTER
CLOSE COMBAT ARMAMENTS CENTER
BENÉT LABORATORIES
WATERVLIET, N.Y. 12189-4050**



APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

DTIC QUALITY INSPECTED 4

20000822 083

DISCLAIMER

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

The use of trade name(s) and/or manufacturer(s) does not constitute an official endorsement or approval.

DESTRUCTION NOTICE

For classified documents, follow the procedures in DoD 5200.22-M, Industrial Security Manual, Section II-19, or DoD 5200.1-R, Information Security Program Regulation, Chapter IX.

For unclassified, limited documents, destroy by any method that will prevent disclosure of contents or reconstruction of the document.

For unclassified, unlimited documents, destroy when the report is no longer needed. Do not return it to the originator.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)		2. REPORT DATE July 2000		3. REPORT TYPE AND DATES COVERED Final
4. TITLE AND SUBTITLE INDEX TO BENET LABORATORIES TECHNICAL REPORTS - 1999			5. FUNDING NUMBERS N/A	
6. AUTHOR(S) R.D. Neifeld				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Benet Laboratories, AMSTA-AR-CCB-O Watervliet, NY 12189-4050			8. PERFORMING ORGANIZATION REPORT NUMBER ARCCB-SP-00013	
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army ARDEC Close Combat Armaments Center Picatinny Arsenal, NJ 07806-5000			10. SPONSORING / MONITORING AGENCY REPORT NUMBER	
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION / AVAILABILITY STATEMENT Approved for public release; distribution unlimited.			12b. DISTRIBUTION CODE	
13. ABSTRACT (Maximum 200 words) This is a compilation of technical reports published by Benet laboratories during 1999.				
14. SUBJECT TERMS Benet Laboratories, Technical Publications, Bibliographies, Abstracts, Document Control Data			15. NUMBER OF PAGES 34	
			16. PRICE CODE	
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED		18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED		19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED
				20. LIMITATION OF ABSTRACT UL

TABLE OF CONTENTS

	<u>Page</u>
LIST OF REPORTS	1
AUTHOR INDEX	3
SUBJECT INDEX	6
AD NUMBERS	12
REPORT DOCUMENTATION PAGES	13

TECHNICAL REPORTS 1999

REPORT NUMBER	TITLE	AUTHOR	DATE
ARCCB-CR-99001	Dynamic Analysis of a 155-mm Cannon Breech	G.P. O'Hara S. VanDyke-Restifo (Benet POC)	Feb 1999
ARCCB-TR-99002	The Use of Thermal Analysis in the Characterization of a Polymer Surface	M.F. Fleszar A. Welty	Mar 1999
ARCCB-TR-99003	Visualization of Cannon Wear Using Ultrasonic Measurements and MATLAB®	J.M. Coyle	Mar 1999
ARCCB-TR-99004	Laser-Ultrasonic Characterization of Electrodeposited Chromium Coatings	B. Knight J. Braunstein J.F. Cox J. Frankel	Mar 1999
ARCCB-TR-99005	A Progress Report on X-Ray Diffraction Measurements on New Low-Thermal Conductivity Thermoelectric Materials	A.P. Hynes S.L. Lee S.B. Schujman G.A. Slack	Apr 1999
ARCCB-SP-99006	Index to Benet Laboratories Technical Reports – 1998	R.D. Neifeld	Apr 1999
ARCCB-TR-99007	Computerized Ultrasonic Gauging	R.W. Reed A. Abbate J. Frankel	May 1999
ARCCB-TR-99008	Thin-Film Density Determination of Tantalum, Tantalum Oxides, and Xerogels by Multiple Radiation Energy Dispersive X-Ray Reflectivity	D. Windover S.L. Lee	May 1999
ARCCB-TR-99009	Bauschinger Effect Design Procedures for Autofrettaged Tubes Including Material Removal and Sachs' Method	A.P. Parker J.H. Underwood D.P. Kendall	May 1999
ARCCB-TR-99010	Analysis of a Piston Experiencing Environmentally-Assisted Cracking as a Result of Compressive Overloading	E. Troiano G.N. Vigilante J.H. Underwood C. Mossey	Jun 1999
ARCCB-TR-99011	Liquid Metal Embrittlement of ASTM A723 Gun Steel by Indium and Gallium	G.N. Vigilante E. Troiano C. Mossey	Jun 1999
ARCCB-TR-99012	Analysis of Engraving and Wear in a Projectile Rotating Band	P.C.T. Chen	Jul 1999
ARCCB-TR-99013	Thermal Damage and Shear Failure of Chromium Plated Coating on an A723 Steel Cannon Tube	J.H. Underwood A.P. Parker	Jul 1999
ARCCB-TR-99014	Thermomechanical Model of Hydrogen Cracking at Heat-Affected Cannon Bore Surfaces	J.H. Underwood G.N. Vigilante E. Troiano	Aug 1999
ARCCB-SP-99015	Proceedings of the Ninth U.S. Army Symposium on Gun Dynamics	E.L. Kathe, Editor	Mar 2000
ARCCB-TR-99016	Gray Layers and the Erosion of Chromium Plated Gun Bore Surfaces	P.J. Cote C. Rickard	Sep 1999

TECHNICAL REPORTS 1999

ARCCB-TR-99017	Analysis of Molten Salt and Sputter-Deposited Coatings on Steel Cylinders	S.L. Lee M. Cipollo D. Windover C. Rickard	Oct 1999
ARCCB-TR-99018	Loading Frequency and Its Effects on the Fatigue Life of A723 Steel	E. Troiano C. Mossey J.H. Underwood	Oct 1999
ARCCB-TR-99019	Fatigue Life Assessment of 155-mm M776 Cannon Tubes	M.J. Audino J.G. Bendick J.J. Keating K.D. Olsen P.M. Weber D.J. Corrigan	Nov 1999
ARCCB-TR-99020	X-Ray Diffraction Techniques and Finite Element Modeling to Control Residual Stress in High-Temperature Pressure Vessels	S.L. Lee P. Chen M. Leach P. Cote D. Windover	Nov 1999
ARCCB-TR-99021	Coating Evaluation Using Analytical and Experimental Dispersion Curves	B. Knight M. Hussain J. Frankel J.F. Cox J. Braunstein P.J. Cote A. Abbate	Nov 1999

AUTHOR INDEX 1999

AUTHOR	REPORT NUMBER
Abbate, A.	ARCCB-TR-99007 ARCCB-TR-99021
Audino, M.J.	ARCCB-TR-99019
Bendick, J.G.	ARCCB-TR-99019
Braunstein, J.	ARCCB-TR-99004 ARCCB-TR-99021
Chen, P.C.T.	ARCCB-TR-99012 ARCCB-TR-99020
Cipollo, M.	ARCCB-TR-99017
Corrigan, D.J.	ARCCB-TR-99019
Cote, P.J.	ARCCB-TR-99016 ARCCB-TR-99020 ARCCB-TR-99021
Cox, J.F.	ARCCB-TR-99004 ARCCB-TR-99021
Coyle, J.M.	ARCCB-TR-99003
Fleszar, M.F.	ARCCB-TR-99002
Frankel, J.	ARCCB-TR-99004 ARCCB-TR-99007 ARCCB-TR-99021
Hussain, B.	ARCCB-TR-99021
Hynes, A.P.	ARCCB-TR-99005
Kathe, E.L.	ARCCB-SP-99015
Keating, J.J.	ARCCB-TR-99019
Kendall, D.P.	ARCCB-TR-99009
Knight, B.	ARCCB-TR-99004 ARCCB-TR-99021

AUTHOR INDEX 1999

Leach, M.	ARCCB-TR-99020
Lee, S.L.	ARCCB-TR-99005 ARCCB-TR-99008 ARCCB-TR-99017 ARCCB-TR-99020
Mossey, C.	ARCCB-TR-99010 ARCCB-TR-99011 ARCCB-TR-99018
Neifeld, R.D.	ARCCB-SP-99006
O'Hara, G.P.	ARCCB-CR-99001
Olsen, K.D.	ARCCB-TR-99019
Parker, A.P.	ARCCB-TR-99009 ARCCB-TR-99013
Reed, R.W.	ARCCB-TR-99007
Rickard, C.	ARCCB-TR-99016 ARCCB-TR-99017
Schujman, S.B.	ARCCB-TR-99005
Slack, G.A.	ARCCB-TR-99005
Troiano, E.	ARCCB-TR-99010 ARCCB-TR-99011 ARCCB-TR-99014 ARCCB-TR-99018
Underwood, J.H.	ARCCB-TR-99009 ARCCB-TR-99010 ARCCB-TR-99013 ARCCB-TR-99014 ARCCB-TR-99018
VanDyke-Restifo, S.	ARCCB-CR-99001
Vigilante, G.N.	ARCCB-TR-99010 ARCCB-TR-99011 ARCCB-TR-99014
Weber, P.M.	ARCCB-TR-99019

AUTHOR INDEX 1999

Welty, A.

ARCCB-TR-99002

Windover, D.

ARCCB-TR-99008

ARCCB-TR-99017

ARCCB-TR-99020

SUBJECT INDEX 1999

SUBJECT	REPORT NUMBER
A723 Steel	ARCCB-TR-99011 ARCCB-TR-99013 ARCCB-TR-99018
Abstracts	ARCCB-SP-99006
Accuracy	ARCCB-SP-99015
Ammunition	ARCCB-CR-99001
Antimony (Stibium)	ARCCB-TR-99005
Autofrettage	ARCCB-TR-99009 ARCCB-TR-99020
Ballistics	ARCCB-SP-99015
Barrel Vibration	ARCCB-SP-99015
Bauschinger Effect	ARCCB-TR-99009
Bibliographies	ARCCB-SP-99006
Bores	ARCCB-TR-99014
Breech Mechanisms	ARCCB-CR-99001
Cannons	ARCCB-CR-99001
Chromium	ARCCB-TR-99004 ARCCB-TR-99010 ARCCB-TR-99013 ARCCB-TR-99016 ARCCB-TR-99021
Coatings	ARCCB-TR-99004 ARCCB-TR-99017 ARCCB-TR-99021
Composite Materials	ARCCB-TR-99005
Compressive Overloading	ARCCB-TR-99010
Computerized Ultrasonic Gauging System (CUGS)	ARCCB-TR-99003
Crack Initiation	ARCCB-TR-99018

SUBJECT INDEX 1999

Crack Propagation	ARCCB-TR-99013
Cracking (Fracturing)	ARCCB-TR-99010 ARCCB-TR-99014
Damage	ARCCB-TR-99013
Density	ARCCB-TR-99008
Dispersion Curves	ARCCB-TR-99021
Dynamics	ARCCB-CR-99001 ARCCB-SP-99015
Electrodeposition	ARCCB-TR-99004
Engraving	ARCCB-TR-99012
Environmental Cracking	ARCCB-TR-99010 ARCCB-TR-99011
Erosion	ARCCB-SP-99015 ARCCB-TR-99016
Extreme Service Condition Pressure	ARCCB-TR-99019
Fatigue Life	ARCCB-TR-99009 ARCCB-TR-99011 ARCCB-TR-99018 ARCCB-TR-99019 ARCCB-TR-99020
Fatigue Tests (Mechanics)	ARCCB-TR-99019
Finite Element Analysis	ARCCB-CR-99001 ARCCB-TR-99010 ARCCB-TR-99012 ARCCB-TR-99020
Fracture (Mechanics)	ARCCB-TR-99014
Fuel Cells	ARCCB-TR-99002
Gallium	ARCCB-TR-99011
Gauging	ARCCB-TR-99007

SUBJECT INDEX 1999

Gun Tubes	ARCCB-TR-99003 ARCCB-TR-99007 ARCCB-TR-99009 ARCCB-TR-99011 ARCCB-TR-99013 ARCCB-TR-99016 ARCCB-TR-99019
Guns	ARCCB-SP-99006 ARCCB-SP-99015
Heating	ARCCB-SP-99015
High Contraction	ARCCB-TR-99016
High Temperature	ARCCB-TR-99020
Hydrogen	ARCCB-TR-99010
Hydrogen Embrittlement	ARCCB-TR-99014
Indexes	ARCCB-SP-99006
Indium	ARCCB-TR-99011
Ion Chromatography	ARCCB-TR-99002
Iridium	ARCCB-TR-99005
Iron Oxides	ARCCB-TR-99016
Iron Sulfides	ARCCB-TR-99016
Laser-Ultrasonics	ARCCB-TR-99004
Lattice Parameters	ARCCB-TR-99005
Liquid Metal Embrittlement	ARCCB-TR-99011
Loading Frequency	ARCCB-TR-99018
Low Contraction	ARCCB-TR-99016
M199 Cannon Breeches	ARCCB-CR-99001
M776 Cannon Tubes	ARCCB-TR-99019
Material Removal	ARCCB-TR-99009

SUBJECT INDEX 1999

MATLAB® Computer Program	ARCCB-TR-99003
Metal Coatings	ARCCB-TR-99004
Molten Salts	ARCCB-TR-99017
Nafion	ARCCB-TR-99002
Nickel	ARCCB-TR-99010
Nondestructive Testing	ARCCB-TR-99008
Pistons	ARCCB-TR-99010
Plastic Deformation	ARCCB-TR-99012
Platinum	ARCCB-TR-99005
Polymers	ARCCB-TR-99002
Pressure Vessels	ARCCB-TR-99009 ARCCB-TR-99010 ARCCB-TR-99018 ARCCB-TR-99020
Projectiles	ARCCB-TR-99012
Protective Coatings	ARCCB-TR-99021
Refractory Coatings	ARCCB-TR-99017
Reports	ARCCB-SP-99006
Residual Stress	ARCCB-TR-99009 ARCCB-TR-99013 ARCCB-TR-99020
Rhodium	ARCCB-TR-99005
Rotating Bands	ARCCB-TR-99012
Sachs' Method	ARCCB-TR-99009
Slicing Effects	ARCCB-TR-99020
Smooth Contact Bonds	ARCCB-TR-99021
Sputtering	ARCCB-TR-99017

SUBJECT INDEX 1999

Statistical Analysis	ARCCB-TR-99019
Steel	ARCCB-TR-99011 ARCCB-TR-99013 ARCCB-TR-99017 ARCCB-TR-99018
Surface Analysis	ARCCB-TR-99002
Symposia	ARCCB-SP-99015
Tantalum	ARCCB-TR-99008 ARCCB-TR-99017 ARCCB-TR-99021
Target Acquisition	ARCCB-SP-99015
Technical Publications	ARCCB-SP-99006
Thermal Analysis	ARCCB-TR-99002
Thermal Stress	ARCCB-TR-99013 ARCCB-TR-99014
Thermoelectricity	ARCCB-TR-99005
Thermomechanics	ARCCB-TR-99014
Thickness Measurements	ARCCB-TR-99007
Thin Films	ARCCB-TR-99008
Tin	ARCCB-TR-99005
Ultrasonics	ARCCB-TR-99003 ARCCB-TR-99004 ARCCB-TR-99007 ARCCB-TR-99019
Vibrations	ARCCB-CR-99001
Visualization	ARCCB-TR-99003
Wall Thickness	ARCCB-TR-99007
Wavelet Techniques	ARCCB-TR-99021
Wear	ARCCB-TR-99003 ARCCB-TR-99012

SUBJECT INDEX 1999

Welded Contact Bonds	ARCCB-TR-99021
White Layers	ARCCB-TR-99016
Xerogels	ARCCB-TR-99008
X-Ray Diffraction	ARCCB-TR-99005
	ARCCB-TR-99020
X-Ray Reflectivity	ARCCB-TR-99008

AD NUMBERS 1999

REPORT NUMBER	AD NUMBER
ARCCB-CR-99001	A360 869
ARCCB-TR-99002	A361 108
ARCCB-TR-99003	A361 642
ARCCB-TR-99004	A362 120
ARCCB-TR-99005	A362 756
ARCCB-SP-99006	A378 175
ARCCB-TR-99007	A364 358
ARCCB-TR-99008	A364 133
ARCCB-TR-99009	A364 640
ARCCB-TR-99010	A364 759
ARCCB-TR-99011	A365 497
ARCCB-TR-99012	A366 887
ARCCB-TR-99013	A367 743
ARCCB-TR-99014	A368 087
ARCCB-SP-99015	A375 229
ARCCB-TR-99016	A369 065
ARCCB-TR-99017	A369 823
ARCCB-TR-99018	A369 960
ARCCB-TR-99019	A370 772
ARCCB-TR-99020	A371 147
ARCCB-TR-99021	A371 275

February 1999

Final

DYNAMIC ANALYSIS OF A 155-MM CANNON BREECH

Contract No. GS-35F-5296H

G. Peter O'Hara

Elmhurst Research
165 Jordan Road
Troy, NY 12181

ARCCB-CR-99001

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

Stephan VanDyke-Restifo – Benet Laboratories Project Engineer. Presented at the 9th U.S. Army Gun Dynamics Symposium, McLean, VA, 17-19 November 1998. Published in proceedings of the symposium.

Approved for public release; distribution unlimited.

This report describes a finite element analysis of the breech closure for the 155-mm M199 cannon, which is normally mounted on the towed howitzer M198. This configuration has an excellent record for reliability in the field and is easy to service. However, when the breech is used in an ammunition test environment, some maintenance problems exist. Our analysis was for a nine-body problem with thirteen contact surfaces, and was solved for both static and dynamic load cases. The two dynamic loads were of similar shape with different loading times. The nine bodies in the model included a facility mount, four major structural components, the obturator seal, and three minor components. The results showed that the major components are normally subjected to quasi-static loading, but under fast "pressure spike" loading, the dynamic effect can be important. This is particularly true for the contact between minor components that can show extreme behavior with the fast-loading rates.

Cannon, Breech, Dynamics, Vibrations, Finite Element

13

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

March 1999

Final

THE USE OF THERMAL ANALYSIS IN THE
CHARACTERIZATION OF A POLYMER SURFACE

AMCMS No. 6226.24.H180.0
PRON No. PJ8K2D1DEX

Mark F. Fleszar and Allison Welty

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99002

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 26th Annual Conference of the North American Thermal Analysis Society, Cleveland, OH.
Published in proceedings of the conference.

Approved for public release; distribution unlimited.

Fuel cells are electrochemical systems that convert hydrogen into electricity without combustion. A proton exchange membrane (PEM) fuel cell power system consists of a polymer membrane, finely dispersed catalyst, and a gas humidifying system. Thermogravimetry (TGA) and differential scanning calorimetry (DSC) are powerful tools that can be used to characterize the physical properties of a polymer membrane. Ion chromatography can monitor the presence of contaminating ions in the aqueous condensate. TGA can easily measure the distribution of metal catalysts on a polymer surface due to the much lower decomposition temperature of the polymer. DSC can be used to measure the concentration of Teflon in a polymer blend by measuring the melting energy.

Fuel Cell, Nafion, Thermal Analysis,
Catalyst, Ion Chromatography

10

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

March 1999

Final

VISUALIZATION OF CANNON WEAR USING
ULTRASONIC MEASUREMENTS AND MATLAB®

AMCMS No. 6226.24.H180.0
PRON No. 4A8A8FYA1ABJ

J. Michael Coyle

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99003

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 9th U.S. Army Gun Dynamics Symposium, McLean, VA, 17-19 November 1998.
Published in proceedings of the symposium.

Approved for public release; distribution unlimited.

CUGS (Computerized Ultrasonic Gauging System), the synergistic use of ultrasonic and computer technology, is used to obtain measurements of a gun tube's bore surface. The bore surface is displayed as a "topographical map" whose colors are related to the physical dimensions of lands and grooves. In this manner, bore wear and erosion can be detected as differences in colors. Visualization software is written in the MATLAB® programming language/environment. All aspects of the process are described with special emphasis on the visualization algorithms and techniques. Also described are examples of typical results obtained from CUGS and the visualization software.

Ultrasonic Gauging, Wear and Erosion, Scientific Visualization,
Centering Algorithm, Newton Iteration

13

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

March 1999

Final

LASER-ULTRASONIC CHARACTERIZATION OF
ELECTRODEPOSITED CHROMIUM COATINGS

AMCMS No. 6111.01.91A1.1

Bryon Knight, Jeffrey Braunstein, Joseph F. Cox, and Julius Frankel

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99004

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 23rd Conference on Quantitative Non-Destructive Evaluation, Snowbird, UT, 23 July 1998.
Published in proceedings of the conference.

Approved for public release; distribution unlimited.

Chromium coatings were electrodeposited onto steel substrates, under controlled conditions. A pulsed laser generated ultrasonic waves in the specimen, and a Michelson interferometer detected the ultrasonic waves at the surface. Signal processing techniques were used to obtain the surface wave velocities, and the various modes are discussed. Conventional piezoelectric techniques were also used for generation and detection of bulk wave velocities to correlate with the surface wave results. A difference technique was used to obtain the bulk measurements: time transit and thickness were measured before and after chromium plating and the velocities evaluated from the respective differences of the data thus obtained.

Ultrasonics, Laser-Ultrasonics, Elastic Properties, Coatings

12

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

April 1999

Final

A PROGRESS REPORT ON X-RAY DIFFRACTION MEASUREMENTS
ON NEW LOW-THERMAL CONDUCTIVITY THERMOELECTRIC MATERIALS

AMCMS No. 6111.01.91A1.1

Anne P. Hynes (RPI, Troy, NY), Sabrina L. Lee,
Sandra B. Schujman (RPI), and Glen A. Slack (RPI)

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99005

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Approved for public release; distribution unlimited.

Thermoelectric devices and materials have potential applications in refrigeration and power generation. An X-ray diffraction study was made documenting the phase and the lattice parameter of both some new thermoelectric compounds and some previously known compositions. The materials contained primarily Ir, Rh, Sb, Sn, and Pt. Improvements in the measurement procedures resulted in improved accuracy in lattice parameter measurements and in peak intensity measurements.

Thermoelectric Materials, Ir, Rh, Sb, Sn, Pt,
Skutterud, Lattice Parameters

21

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

April 1999

Final

**INDEX TO BENET LABORATORIES
TECHNICAL REPORTS - 1998**

N/A

R.D. Neifeld

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-SP-99006

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Approved for public release; distribution unlimited.

This is a compilation of technical reports published by Benet Laboratories during 1998.

Benet Laboratories, Technical Publications, Bibliographies, Abstracts, Document Control Data

31

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

May 1999

Final

COMPUTERIZED ULTRASONIC GAUGING

AMCMS No. 6111.01.91A1.1

Robert W. Reed (East Stroudsburg University, East Stroudsburg, PA),
A. Abbate*, and J. Frankel

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99007

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Submitted to *Research in Nondestructive Evaluation*, A Journal of the American Society for Nondestructive Testing.
*Current Address: Textron Systems Division, 201 Lowell Street, Wilmington, MA 01887.

Approved for public release; distribution unlimited.

A high-precision ultrasonic gauging system has been designed and implemented for use on a CNC lathe. The system uses a PC along with a number of plug-in cards to generate, receive, and process ultrasonic signals. The system has been reliably used both during and after machining operations. It is capable of simultaneous measurement of wall thickness, runout, outer diameter radius, inner diameter radius, and concentricity of the inner diameter and outer diameter. Data densities of 2000 measurements per revolution of all parameters can be achieved. Data can be acquired at lathe spindle speeds that keep the outside part surface moving at less than about 2000 surface feet per minute. A real-time, pseudo-color, image of the wall thickness is provided during operation. The system can receive setup and operational instructions from the lathe CNC so that operation can be accomplished with very little operator involvement.

Ultrasonics, Gauging, Thickness Measurements,
Wall Thickness, Gun Tubes

20

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

May 1999

Final

THIN-FILM DENSITY DETERMINATION OF TANTALUM, TANTALUM OXIDES, AND
XEROGELS BY MULTIPLE RADIATION ENERGY DISPERSIVE X-RAY REFLECTIVITY

AMCMS No. 6111.01.91A1.1

D. Windover and S.L. Lee

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99008

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 47th Annual Denver X-Ray Conference, Sponsored by International Centre for Diffraction Data,
Colorado Springs, CO, 3-7 August 1998. Published in *Advances in X-Ray Analysis*.

Approved for public release; distribution unlimited.

X-ray reflectivity provides a nondestructive technique for measuring density in thin films. A conventional laboratory, Bragg-Brentano geometry diffractometer was employed to show the generalized feasibility of this technique. X-ray tubes with chromium, copper, and molybdenum targets were used to provide a large overlap of energies for density fitting. X-ray tube alignment and sample alignment were explored to find a self-consistent measurement technique. The real and complex indices for tantalum, TaO_x , and porous SiO_2 , also known as "xerogel," were calculated and used in a reflectivity-fitting routine. The density results from multiple energies provided a self-checking method for true density extrapolation from misaligned samples. Density results for the xerogel films were compared with measurements by Rutherford backscattering spectrometry and by optical ellipsometry, and showed consistency within errors.

X-Ray Reflectivity, Density, Tantalum,
Tantalum Oxides, Energy Dispersive

14

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

May 1999

Final

**BAUSCHINGER EFFECT DESIGN PROCEDURES FOR AUTOFRETTAGED
TUBES INCLUDING MATERIAL REMOVAL AND SACHS' METHOD**

AMCMS No. 6226.24.H181.0

Anthony P. Parker (Royal Military College of Science, Cranfield University,
Swindon, UK), John H. Underwood, and David P. Kendall (Consultant, Troy, NY).

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99009

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

To be presented at the ASME Pressure Vessels and Piping Conference, Boston, MA, 1-5 August 1999.
To be published in proceedings of the conference.

Approved for public release; distribution unlimited.

Autofrettage is used to introduce advantageous residual stresses into pressure vessels and to enhance their fatigue lifetimes. The Bauschinger effect serves to reduce the yield strength in compression as a result of prior tensile plastic overload and can produce lower compressive residual hoop stresses near the bore than are predicted by 'ideal' autofrettage solutions (elastic/perfectly plastic without Bauschinger effect). A complete analysis procedure is presented which encompasses representation of elastic-plastic uniaxial loading material behavior and of reverse-loading material behavior as a function of plastic strain during loading. Such data are then combined with some yield criterion to accurately predict elastic-plastic residual stress fields within an autofrettaged thick cylinder. Pressure for subsequent re-yielding of the tube is calculated. The numerical procedure is further used to determine residual stress fields after removal of material from inside diameter (ID) and/or outside diameter (OD), including the effects of any further plasticity. A specific material removal sequence is recommended. It is shown that Sachs' experimental method, which involves removing material from the ID, may very significantly overestimate autofrettage residual stresses near the bore. Stress ranges and stress intensity factors for cracks within such stress fields are calculated together with the associated fatigue lifetimes as such cracks propagate under cyclic pressurization. The loss of fatigue lifetime resulting from the Bauschinger effect is shown to be extremely significant.

Bauschinger Effect, Autofrettage, Gun Tubes, Sachs' Method,
Residual Stresses, Fatigue Life, Pressure Vessels

11

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

June 1999

Final

ANALYSIS OF A PISTON EXPERIENCING ENVIRONMENTALLY-
ASSISTED CRACKING AS A RESULT OF COMPRESSIVE OVERLOADING

AMCMS No. 4221.23.0000.0

E. Troiano, G.N. Vigilante, J.H. Underwood, and C. Mossey

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99010

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the International Conference on Mechanical Behavior of Materials, Victoria, British Columbia, Canada, 16-21 May 1999.
Published in proceedings of the conference.

Approved for public release; distribution unlimited.

A piston used in service in a closed-ended pressure vessel, as a component of the seal for the vessel, cracked after as few as two high-pressure loading cycles. As a further complication, the finite element analysis was predicting compression on the cracked piston face during the loading cycle. The cracks in the piston emanated in a radial fashion and were measured at 1.5-mm deep. Upon subsequent loading, the cracks grew in length (in large incremental advances), but did not propagate any deeper than the initial 1.5-mm. In all instances the robust design did not leak. A closer look at the finite element analysis revealed that the piston, made from Maraging 200 steel, was loaded in compression to above the compressive yield point of the material. The initial loading set up a residual tensile stress as a result of the compressive yielding. On the next successive loading, this tensile residual stress field, coupled with the hydrogen-rich products in the pressure vessel and a highly susceptible material, resulted in cracking. The fact that the cracks were only 1.5-mm deep suggests that this was the extent of the compressive yielding, and that the cracks arrested themselves once the neutral axis or zero stress was encountered. The fracture morphology of the cracks revealed that they were intergranular in nature, and likely to be the result of hydrogen-induced cracking. At this point in the program the design of the piston was firmly established, so the only alternatives were to prevent the hydrogen from getting to the susceptible material, or to change to a less susceptible material. Consideration of the second alternative revealed no material that possessed the unique combinations of strength, toughness, hydrogen resistance, or producibility that were required. Therefore, plating of the piston with various nickel and chromium combinations was investigated. Laboratory tests were devised using a modified bolt-loaded compact specimen for conducting plating studies. The specimens were loaded near the yield strength of the material and exposed to a hydrogen-rich environment. After over 300 hours of exposure, no cracking had occurred in any of the electroplated nickel specimens. These results were then applied to the piston and placed into service. The piston currently has over 700 high-pressure loading cycles with no cracks observed.

Environmentally-Assisted Cracking, Hydrogen, Pressure Vessels
Compressive Overload, Nickel Coating

12

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

June 1999

Final

**LIQUID METAL EMBRITTLEMENT OF ASTM A723
GUN STEEL BY INDIUM AND GALLIUM**

AMCMS No. 8Y10.00.0000.0

Gregory N. Vigilante, Edward Troiano, and Charles Mossey

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99011

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Approved for public release; distribution unlimited.

An investigation was performed to determine the effects of gallium and indium on the liquid metal embrittlement of ASTM A723 gun steel. Liquid metal embrittlement tests were conducted slightly above the melting temperature of the embrittling metal in an elevated temperature furnace coupled to an Instron mechanical tester. Low cycle fatigue and monotonic tensile testing of notched tensile specimens were performed. In addition, the effect of strain rate on the embrittlement of ASTM A723 by gallium was evaluated. The low cycle fatigue tests showed a high sensitivity to liquid metal embrittlement; both the gallium and the indium significantly degraded the fatigue life of the gun steel. Monotonic tests on ASTM A723 also showed an embrittling effect with both gallium and indium, although the effect was less severe than when tested in low cycle fatigue.

Liquid Metal Embrittlement, Environmental Cracking, Gallium
Indium, Gun Steel, High-Strength Steels, ASTM A723

21

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

July 1999

Final

ANALYSIS OF ENGRAVING AND WEAR
IN A PROJECTILE ROTATING BAND

AMCMS No. 6226.24.H191.1

Peter C.T. Chen

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99012

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 9th U.S. Army Gun Dynamics Symposium, McLean, VA, 17-19 November 1998.
Published in proceedings of the symposium

Approved for public release; distribution unlimited.

A large deformation analysis of the engraving process and wear in a projectile rotating band is considered by using the finite element program ABAQUS. The tube and the projectile are assumed to be rigid, and the bore of the tube is assumed to be smooth and axisymmetric. An elastic-plastic material model is chosen for the copper band, which remains attached to the projectile, and an appropriate coefficient of sliding friction is chosen. The magnitude and distribution of the contact pressure between the band and the tube are obtained during engraving. The band pressure is large with severe plastic deformation occurring in the band.

Engraving, Wear, Projectile, Rotating Band, Plastic Deformation

16

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

July 1999

Final

**THERMAL DAMAGE AND SHEAR FAILURE OF CHROMIUM
PLATED COATING ON AN A723 STEEL CANNON TUBE**

PRON No. F18X2011M21A

John H. Underwood and Anthony P. Parker (Royal Military
College of Science, Cranfield University, Swindon, UK)

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99013

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

To be presented at the ASME Pressure Vessels and Piping Conference, Boston, MA, 1-5 August 1999.
To be published in proceedings of the conference.

Approved for public release; distribution unlimited.

Degradation of the electroplated chromium coating at the bore of A723 steel cannon barrels is characterized here following cannon firing and used to model the coating failure process. Transient thermal stresses due to firing are calculated using one-dimensional heat flow analysis and used as input to a shear failure model of the coating/substrate couple. The cracking array that develops in the coating and substrate with repeated thermal cycles, the configuration of cracked segments of the coating, and the elevated temperature properties of the coating and substrate are considered in the shear failure model. Accordingly, the coating failure behavior predicted from the model is compared with the observations of coating failure mechanisms from actual fired cannon tubes. The results of the investigation show that growth of hydrogen cracks in the steel under the chromium coating allows broadening of cracks in the coating, and subsequent shear failure of the steel under a segment of coating due to transient thermal stresses. Loss of coating segments then leads to rapid hot gas erosion of the steel and loss of function of the cannon tube. The objective is to model the final critical phase of thermal damage imparted to a chromium coating on a cannon bore that leads to the separation of a segment of coating.

Thermal Damage, Chromium Plating, Alloy Steel, Cannon Tube,
Hydrogen Cracks, Thermal Stress, Residual Stress

18

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

August 1999

Final

**THERMOMECHANICAL MODEL OF HYDROGEN CRACKING
AT HEAT-AFFECTED CANNON BORE SURFACES**

PRON No. 99797WR00542

J.H. Underwood, G.N. Vigilante, and E. Troiano

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99014

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the International Workshop on Hydrogen Management for Welding Applications, Ottawa, Canada, 6-8 October 1998.
Published in proceedings of the workshop.

Approved for public release; distribution unlimited.

Two examples of hydrogen cracking in the heat-affected region of fired cannons are given, including metallographic evidence of damage at various depths near the bore surface. The depth of steel transformation due to firing is used to verify near-bore temperature distributions and transient and residual stress distributions calculated using classic one-dimensional heat flow analysis. Predicted depths of thermal damage and hydrogen cracks compare well with observed depths for different crack orientations and firing temperatures. Laboratory fracture mechanics tests using bolt-load compact specimens are described, including crack growth and blunt-notched tests in acid-hydrogen environments. The utility of the thermal and fracture mechanics analyses and the laboratory fracture mechanics tests used with cannons are discussed for weld applications.

Thermomechanical Model, Cannon Bore, Thermal Stress,
Hydrogen Cracking, Fracture Mechanics

15

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

March 2000

Final

PROCEEDINGS OF THE NINTH U.S. ARMY
SYMPOSIUM ON GUN DYNAMICS

AMCMS No. 6226.24.H191.1

Eric L. Kathe, Editor

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-SP-99015

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the Ninth U.S. Army Symposium on Gun Dynamics, McLean, VA, 17-19 November 1998.

This symposium was sponsored by Benet Laboratories and the U.S. Army Research Office.

Note the report number was assigned in advance of report publication. The final copy of this publication was approved in March 2000.

Approved for public release; distribution unlimited.

This publication represents a compilation of the technical papers concerning modeling, analyses, design, measurements, and instrumentation of gun dynamics. The authors represent a cross section of the scientific and technical community, including universities, industrial, and government research laboratories.

Ballistics, Barrel Vibration, Dynamics, Precision, Controls,
Target Acquisition, Accuracy, Heating, Erosion

519

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

September 1999

Final

GRAY LAYERS AND THE EROSION OF
CHROMIUM PLATED GUN BORE SURFACES

AMCMS No. 6226.24.H191.1

Paul J. Cote and Christopher Rickard

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99016

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Approved for public release; distribution unlimited.

The present report describes observations and analyses in a survey study of erosion damage in chromium plated gun bore surfaces. Sections of three fired chromium plated 120-mm M256 gun tubes and two 155-mm gun tubes (M199 and XM297) were examined by optical microscopy, laser scanning confocal microscopy (LSCM), and electron microprobe analyses. These tubes experienced significant erosion damage and chromium loss. A rifled portion of the 155-mm M199 tube was plated with low contractile (LC) chromium and the 155-mm XM297 and 120-mm M256 tubes were plated with high contractile (HC) chromium.

New insights regarding the erosion process and the origin of chromium loss are obtained by investigation of the initial damage to the steel at the tips of the fine cracks in the chromium. Reaction products from gas-metal interactions at the gun bore surface are normally difficult to find because of gas wash effects. Examination of unetched specimens from a variety of fired tubes shows that these products remain in place in the relatively protected regions beneath the chromium when chromium crack widths are small. The initial damage is manifested as gray layers or gray regions in the steel at the tips of the fine chromium cracks. Electron microprobe analyses indicate that these gray layers are composed of iron sulfide, iron oxide, or mixtures of the two compounds.

Erosion, High Contractile Chromium, Low Contractile Chromium,
Iron Sulfide, Iron Oxide, Chromium Spallation, White Layers

18

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

October 1999

Final

ANALYSIS OF MOLTEN SALT AND SPUTTER-
DEPOSITED COATINGS ON STEEL CYLINDERS

AMCMS No. 6111.01.91A1.1

S.L. Lee, M. Cipollo, D. Windover, and C. Rickard

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99017

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 26th International Conference on Metallurgical Coatings and Thin Films, San Diego, CA, 12-16 April 1999.
Published in *Surface Coatings and Technology*.

Approved for public release; distribution unlimited.

Prototype tantalum coatings, electrochemically deposited from a molten salt onto 20-mm interior bore steel liners, exhibited superior wear and erosion behavior compared to chromium coatings. The liners were subjected to cyclic exposures of high temperature, pressure, and an aggressive chemical environment. X-ray analysis of the coatings revealed a low-hardness, randomly-oriented, body-centered-cubic, α -phase tantalum. Formation of tantalum oxides (predominantly Ta_2O_5), swaging due to the low-hardness of the coatings, a 2- μ m layer consisting of tantalum and carbon at the tantalum/steel interface, and surface compressive residual stresses were observed. Cylindrical magnetron sputtering systems were constructed to coat 45-mm interior bore steel cylinders to protect them from wear and erosion. X-ray diffraction, scanning electron microscopy, photomicrography, and hardness analysis of several sputter-deposited tantalum specimens revealed coatings consisting of soft body-centered-cubic α -phase and hard tetragonal β -phase tantalum.

Molten Salt Deposition, Cylindrical Magnetron Sputtering Deposition,
Tantalum, Thick Refractory Coatings

23

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

October 1999

Final

LOADING FREQUENCY AND ITS EFFECTS
ON THE FATIGUE LIFE OF A723 STEEL

AMCMS No. 4221.23.0000.0

E. Troiano, C. Mossey, and J.H. Underwood

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99018

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Approved for public release; distribution unlimited.

The fatigue life of pressure vessels manufactured from two strength levels (166 Ksi and 190 Ksi) of A723 steel has been modeled, and the life predictions using the model have verified that a field loading cycle is equivalent to a laboratory pressurization loading cycle. One key assumption in the model is that a minimum crack initiator must be present in order to attain a one-to-one correlation. If the minimum crack initiator is not present, there will be a large error between laboratory and field loading when predicting final fatigue failure. This study shows that a crack initiator greater than about 0.019 inch (for 166 Ksi yield strength steel) and 0.008 inch (for 190 Ksi yield strength steel) will result in the one-to-one correlation that is sought. No attempt has been made to model environmental effects that can greatly affect the results presented here.

Frequency, Fatigue Life, Life Prediction, Crack Initiation

7

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

November 1999

Final

**FATIGUE LIFE ASSESSMENT OF
155-MM M776 CANNON TUBES**

AMCMS No. 6226.24.H191.1

Michael J. Audino, James G. Bendick, John J. Keating,
Kenneth D. Olsen, Paul M. Weber, and Daniel J. Corrigan

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99019

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Approved for public release; distribution unlimited.

Benet Laboratories has the responsibility for safe fatigue life (durability) testing of cannon system components. This safe fatigue or service life evaluation is accomplished by conducting constant amplitude fatigue testing in a laboratory setting. One such cannon component that requires testing is the gun tube. After each tube has received the required number of live fire rounds necessary to generate initial cracking at the bore surface (also known as heat-check cracking), it is brought to the laboratory for final hydraulic fatigue testing.

A sample size of two 155-mm M776 gun tubes was hydraulically fatigue tested to failure at Benet Laboratories to assist in determining the safe fatigue life for the weapon. This report contains the results of the fatigue tests conducted on the subject tubes, including material inspections, failure lives, and the resulting value for safe fatigue life of the XM776 gun tube.

XM776 Cannon, Final Safe Fatigue Life, Fatigue Testing, Extreme Service
Condition Pressure, Ultrasonic Inspection, Statistical Analysis

22

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

November 1999

Final

**X-RAY DIFFRACTION TECHNIQUES AND FINITE ELEMENT MODELING
TO CONTROL RESIDUAL STRESS IN HIGH-TEMPERATURE PRESSURE VESSELS**

AMCMS No. 6111.01.91A1.1

S.L. Lee, P. Chen, M. Leach, P. Cote, and D. Windover

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99020

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 1999 Society for Experimental Mechanics Conference, Cleveland, OH, 7-9 June 1999.
Published in proceedings of the conference.

Approved for public release; distribution unlimited.

Manufacturing operations, such as swage autofrettage, shot peening, and overload processes, have been used to impart advantageous residual stresses to improve fatigue life in components used in high-temperature pressure vessels. Both experimental and modeling techniques depend on the geometry and processing history of the component under investigation. This report compares x-ray diffraction residual stress measurements in a swage autofrettaged steel cylinder with finite element modeling results of a cylinder with a given bore expansion. The report also examines an analytical model of a cylinder under internal pressure, including both Bauschinger and strain-hardening effects. From a simple swaged cylinder to a complicated perforated cylinder and overstrained and shot-peened multiple-lug breech structure, control of residual stresses through experimental and modeling efforts is vital in the design of pressure vessels. This report discusses the role of slicing operations, surface polishing, surface roughness, and resolution effects in structures that contain high stress gradients.

Pressure Vessels, Residual Stress, Surface Roughness Effect,
Surface Polishing Effect, Surface Stress Gradients, Slicing Effect

19

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

November 1999

Final

COATING EVALUATION USING ANALYTICAL
AND EXPERIMENTAL DISPERSION CURVES

PRON No. 8LRMFARD77

B. Knight, M. Hussain, J. Frankel, J.F. Cox, J. Braunstein,
P.J. Cote, and A. Abbate (Textron Systems, Wilmington, MA)

U.S. Army ARDEC
Benet Laboratories, AMSTA-AR-CCB-O
Watervliet, NY 12189-4050

ARCCB-TR-99021

U.S. Army ARDEC
Close Combat Armaments Center
Picatinny Arsenal, NJ 07806-5000

Presented at the 26th Annual Review of Progress in Quantitative Nondestructive Evaluation, Montreal, Canada, 25-31 July 1999.
Published in *Review of Progress in Quantitative Nondestructive Evaluation*.

Approved for public release; distribution unlimited.

Well-bonded or "welded" contact and poorly bonded or "smooth" contact bonds were studied. As examples of welded contact bonds, we used sputtered tantalum and electrodeposited high contraction chromium coatings that were deposited onto steel substrates under controlled conditions. In order to simulate smooth contact coatings, thin sheets of nickel and tantalum were epoxied to copper and steel substrates, respectively. We used the method originated by Cielo et al. to gather data consisting of laser generation of the surface waves in an annular ring and laser detection in the center. Wavelet techniques were used on the surface wave-detected signals in order to obtain the experimental dispersion (velocity-frequency) curves. The experimental dispersion curves were compared to theoretical curves to give insight into the bond quality. It was found that the experimental results correlated well with the theory for the welded case.

Coatings, Dispersion Curves, Welded Contact Bonds, Smooth
Contact Bonds, Wavelet Techniques, Tantalum, Chromium

11

UNCLASSIFIED

UNCLASSIFIED

UNCLASSIFIED

UL

TECHNICAL REPORT INTERNAL DISTRIBUTION LIST

	<u>NO. OF COPIES</u>
TECHNICAL LIBRARY ATTN: AMSTA-AR-CCB-O	5
TECHNICAL PUBLICATIONS & EDITING SECTION ATTN: AMSTA-AR-CCB-O	3
OPERATIONS DIRECTORATE ATTN: SIOWV-ODP-P	1
DIRECTOR, PROCUREMENT & CONTRACTING DIRECTORATE ATTN: SIOWV-PP	1
DIRECTOR, PRODUCT ASSURANCE & TEST DIRECTORATE ATTN: SIOWV-QA	1

NOTE: PLEASE NOTIFY DIRECTOR, BENÉT LABORATORIES, ATTN: AMSTA-AR-CCB-O OF ADDRESS CHANGES.

TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST

	<u>NO. OF COPIES</u>		<u>NO. OF COPIES</u>
DEFENSE TECHNICAL INFO CENTER		COMMANDER	
ATTN: DTIC-OCA (ACQUISITIONS)	2	ROCK ISLAND ARSENAL	
8725 JOHN J. KINGMAN ROAD		ATTN: SIORI-SEM-L	1
STE 0944		ROCK ISLAND, IL 61299-5001	
FT. BELVOIR, VA 22060-6218			
COMMANDER		COMMANDER	
U.S. ARMY ARDEC		U.S. ARMY TANK-AUTMV R&D COMMAND	
ATTN: AMSTA-AR-WEE, BLDG. 3022	1	ATTN: AMSTA-DDL (TECH LIBRARY)	1
AMSTA-AR-AET-O, BLDG. 183	1	WARREN, MI 48397-5000	
AMSTA-AR-FSA, BLDG. 61	1	COMMANDER	
AMSTA-AR-FSX	1	U.S. MILITARY ACADEMY	
AMSTA-AR-FSA-M, BLDG. 61 SO	1	ATTN: DEPT OF CIVIL & MECH ENGR	1
AMSTA-AR-WEL-TL, BLDG. 59	2	WEST POINT, NY 10966-1792	
PICATINNY ARSENAL, NJ 07806-5000			
DIRECTOR		U.S. ARMY AVIATION AND MISSILE COM	
U.S. ARMY RESEARCH LABORATORY		REDSTONE SCIENTIFIC INFO CENTER	2
ATTN: AMSRL-DD-T, BLDG. 305	1	ATTN: AMSAM-RD-OB-R (DOCUMENTS)	
ABERDEEN PROVING GROUND, MD		REDSTONE ARSENAL, AL 35898-5000	
21005-5066			
DIRECTOR		COMMANDER	
U.S. ARMY RESEARCH LABORATORY		U.S. ARMY FOREIGN SCI & TECH CENTER	
ATTN: AMSRL-WM-MB (DR. B. BURNS)	1	ATTN: DRXST-SD	1
ABERDEEN PROVING GROUND, MD		220 7TH STREET, N.E.	
21005-5066		CHARLOTTESVILLE, VA 22901	
COMMANDER			
U.S. ARMY RESEARCH OFFICE			
ATTN: TECHNICAL LIBRARIAN	1		
P.O. BOX 12211			
4300 S. MIAMI BOULEVARD			
RESEARCH TRIANGLE PARK, NC 27709-2211			

NOTE: PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH, DEVELOPMENT, AND ENGINEERING CENTER,
BENÉT LABORATORIES, CCAC, U.S. ARMY TANK-AUTOMOTIVE AND ARMAMENTS COMMAND,
AMSTA-AR-CCB-O, WATERVLIET, NY 12189-4050 OF ADDRESS CHANGES.

DEPARTMENT OF THE ARMY
ARMAMENT RESEARCH, DEVELOPMENT AND ENGINEERING CENTER
BENET LABORATORIES, CCAC
US ARMY TANK-AUTOMOTIVE AND ARMAMENTS COMMAND
WATERVLIET, N.Y. 12189-4050

OFFICIAL BUSINESS
AMSTA-AR-CCB-O
TECHNICAL LIBRARY